Research Report

# Selective Reduction of NO over Pt-Mo Catalysts under Lean Static Conditions

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### **Abstract**

The selective reduction of NO<sub>x</sub> on various PtMoX-catalysts (X: Li, Na, K, Mg and Ca) loaded on metal oxides such as SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, ZSM-5 and silicalite was studied in simulated exhaust gases from an automotive lean-burn engine and a stoichiometric engine and compared with that on PtMo/SiO<sub>2</sub>, PtNa/SiO<sub>2</sub>, and Pt/SiO<sub>2</sub> catalysts. The temperature window for the selective reduction of NO<sub>x</sub> on the PtMoLi-, PtMoNa- and PtMoK-catalysts loaded on SiO<sub>2</sub> was found to be wider and to shift to a higher temperature than that on the other catalysts under

lean static conditions. The redox ratio window, in which three-way activity occurred on a PtMoNa catalyst loaded on SiO<sub>2</sub>, was also found to be wider than that on PtMo/SiO<sub>2</sub>, catalysts and Pt/SiO<sub>2</sub> around the stoichiometric point. On the other hand, XPS, IR and CO adsorption data indicated that the oxidation of Pt on PtMoNa/SiO<sub>2</sub> catalysts was depressed by the added Mo and Na even under excess oxygen conditions, so that the reaction characteristics of the PtMoNa/SiO<sub>2</sub> catalysts were improved.

Keywords

Exhaust catalysts, Molybdenum, NO selective reduction, Platinum, Silica, Sodium

### 1. Introduction

Lean-burn gasoline and diesel engines achieve high fuel economy using a higher air/fuel ratio (A/F). However, it is difficult to remove NO<sub>x</sub> in exhaust gases from these engines under excess oxygen conditions. Selective catalytic reduction of NO<sub>x</sub> under such excess oxygen conditions has been an object of study for several years. Extensive research has been carried out to develop a catalyst suitable for practical use. It has been reported that copper ion-exchanged zeolites such as Cu-ZSM-5 <sup>1-5)</sup> are efficient for the reduction of NO<sub>x</sub>. Some noble metal catalysts <sup>6-13)</sup> are found to be superior in durability to the copper

zeolite system under both oxidizing and reducing conditions.

It is well-known that supported noble metal catalysts are active for the reaction of NO with  $H_2$ , CO or  $NH_3^{14,\ 15)}$ . Three-way catalysts (TWCs) which consist of noble metals and several oxides have been used for the catalytic control of automotive emissions. Such catalysts function efficiently in engine exhaust oscillating just rich of the stoichiometric air-to-fuels (A/F) ratio in a narrow A/F window, so that conversion of  $NO_x$ , CO and hydrocarbons (HC) occurs, but do not work in a lean static exhaust  $^{16)}$ . Recently, a new concept TWC, which removes  $NO_x$ , CO and HC under rich-

lean dynamic conditions, has been developed and practically used  $^{17, 18)}$ . However the new concept TWC is not expected to remove  $NO_x$  under lean static conditions.

Bimetallic Pt-Mo and Pd-Mo catalysts have been demonstrated to modify the catalysis of each component and to create new catalytic properties: such as hydrogenolysis  $^{19-21)}$ , hydrogenation  $^{22)}$ , NO<sub>x</sub> reduction  $^{23-25)}$ , and unusual characterization  $^{26-28)}$ .

The purpose of this study was to examine  $NO_x$  reduction and three-way activity of the PtMocatalysts with various additives and supports<sup>29)</sup>. Another purpose was to present XPS, IR and CO adsorption results to clarify the state of Pt on these catalysts in the simulated model gases<sup>34)</sup>.

# 2. Experimental

## 2. 1 Catalyst preparation

Sixteen catalysts composed of Pt, MoO<sub>3</sub>, basic additives and various metal oxides were prepared by an impregnation method as summarized in **Table 1**. The PMNS2 catalyst was prepared by the same method using SiO<sub>2</sub> powder (AEROSIL TT600, Nippon Aerosil Corp., 200m<sup>2</sup>/g), CH<sub>3</sub>COONa·3H<sub>2</sub>O (Wako Pure Chemical Industries), (NH<sub>4</sub>)<sub>6</sub>Mo<sub>7</sub>O<sub>27</sub>·4H<sub>2</sub>O (Wako Pure Chemical Industries) and Pt(NH<sub>3</sub>)<sub>2</sub>(NO<sub>2</sub>)<sub>2</sub> (Tanaka Precious Metal Co.), and calcined at 500°C for 3h in flowing 10% H<sub>2</sub> / N<sub>2</sub>. The Pt, MoO<sub>3</sub> and Na<sub>2</sub>O loading amounts were 1.67wt%, 12.3wt% and 0.1wt%, respectively. Other catalysts were prepared in the same way as described above starting from the corresponding additives and supports as shown in Table 1. The prepared catalysts were pressed into disks and pulverized to a 300~700 µm size.

### 2. 2 Activity measurement

The laboratory reactor system used in this experiment is similar to the previously described system<sup>30)</sup>. Catalytic activity data were obtained using a conventional fixed-bed flow reactor at atmospheric pressure. A quartz tube with an inner diameter of 18mm was chosen as the reactor tube. 0.5 g catalyst (~1 cm³) was placed on a quartz filter at the middle part of the reactor. The upper part of the catalyst bed was packed with 7 cm³ of inactive SiC spheres (3 mm o.d.) for preheating the feed gas. Furnace temperature was controlled with a maximum variation of 2°C by an automatic temperature controller. The gas leaving the reactor was led to a condenser to remove the water vapor.

The remaining components were continuously analyzed by nondispersive infrared (CO and  $CO_2$ ), flame ionization (hydrocarbon, HC), magnetic susceptibility ( $O_2$ ), and chemiluminescence ( $NO_x$ ) equipped with a gas analyzer (Horiba MEXA-8120).

We chose propene to simulate a hydrocarbon in the feedstream in order to measure the activity of the prepared catalysts under hard conditions.

The redox ratio, S, used to identify the redox characteristic of the model gas mixtures is defined as

$$S = \frac{NO + 2 \times O_2}{H_2 + CO + 9 \times C_3 H_6}$$
 (1)

When S < 1.0, S = 1.0, and S > 1.0, the composition of the feedstream is net reducing, stoichiometric, and net oxidizing, respectively.

The feed compositions and reaction conditions used in this study were as follows:(1) The simulated oxidizing feedstream consisted of 4.3 %  $O_2$ , 0.12 % NO, 800 ppm  $C_3H_6$ , 0.12 % CO, 400 ppm  $H_2$ , 12.3 %  $CO_2$ , 3 %  $H_2O$  and the balance of  $N_2$ . This mixture corresponded to S = 9.91 and simulated an A/F ratio of 18 (lean mixture). For each light-off test, catalysts were exposed to the simulated exhaust at 3.3 l/min while the temperature was decreased from  $600^{\circ}C$  to  $100^{\circ}C$  at  $5^{\circ}C$  /min and at  $9.91 \times 10^{-3}$ 

Table 1 Catalyst formulations.

Catalyst	Pt loading (wt%)	MoO <sub>3</sub> loading (wt%)	ad	ditive loading (wt%)	Support
PMNS1	1.67	12.3	Na <sub>2</sub> O	0.05	SiO <sub>2</sub>
PMNS2	1.67	12.3	$Na_2O$	0.1	$SiO_2$
PMNS3	1.67	12.3	$Na_2O$	1.0	$SiO_2$
PMLS	1.67	12.3	Li <sub>2</sub> O	0.1	$SiO_2$
PMKS	1.67	12.3	$K_2O$	0.1	$SiO_2$
PMMS	1.67	12.3	MgO	0.1	$SiO_2$
PMCS	1.67	12.3	CaO	0.1	$SiO_2$
PMNA	1.67	12.3	$Na_2O$	0.1	$Al_2O_3$
PMNT	1.67	12.3	$Na_2O$	0.1	$TiO_2$
PMNZ	1.67	12.3	$Na_2O$	0.1	ZSM-5
PMNs	1.67	12.3	$Na_2O$	0.1	silicalite
PMS	1.67	12.3	-	0	$SiO_2$
PNS	1.67	0	$Na_2O$	0.1	$SiO_2$
PS	1.67	0	-	0	$SiO_2$
MS	0	12.3	-	0	$SiO_2$
NS	0	0	$Na_2O$	0.1	$SiO_2$

g·sec/cc W/F.

(2) The simulated exhaust gases for the *S*-scan were composed of  $0.40 \sim 1.21 \% O_2$ , 0.12 % NO,  $490 \sim 620 \text{ ppm C}_3H_6$ ,  $0.45 \sim 1.50 \% CO$ ,  $0.15 \sim 0.50 \% H_2$ ,  $10.0 \% CO_2$ ,  $3.0 \% H_2O$  and the balance of  $N_2$ . Catalytic activities of the catalysts were expressed as percent conversion of  $NO_x$ . Conversion data were measured at  $450 ^{\circ}C$  and  $9.91 \times 10^{-3} \text{ g·sec/cc W/F}$ . The activity measurements as a function of *S* are designated as the *S*-scan. In this experiments, *S* is changed gradually from reducing to oxidizing conditions by adjusting the  $O_2$ ,  $C_3H_6$ , CO and  $H_2$  contents at the inlet of the reactor.

# 2. 3 Infrared spectroscopy

IR spectra were recorded on a JASCO FTIR-8900 spectrometer equipped with an MCT detector and a diffuse reflectance IR cell. The catalyst sample placed in an in situ IR cell with a KBr window was pretreated at 400°C for 1 h in flowing 7 %  $O_2/N_2$  ( $O_2$  pretreatment), and then cooled to  $200^{\circ}$ C. CO was adsorbed at  $200^{\circ}$ C in flowing 0.28% CO/ $N_2$  and the IR spectra were measured. The IR spectra of CO adsorbed on the sample were obtained by subtracting the spectra before CO adsorption from those after that. In another IR measurement, other catalyst samples were pretreated in flowing  $N_2$  ( $N_2$  pretreatment) and 7 %  $H_2/N_2$  ( $H_2$  pretreatment) by the same procedure as mentioned above except for pretreating in flowing 7 %  $O_2/N_2$ .

# 2. 4 X-ray Photoelectron spectroscopy (XPS)

In-situ XPS measurements were performed on a V.G. SCIENTIFIC ESCALAB MK III with Mg-K $\alpha$  X-rays. The catalyst sample was placed on a grid and preheated under  $1\times 10^{-7}$  torr  $O_2$  pressure at 400°C for 1 h. The preheated sample was cooled to room temperature under the same atmosphere and then transferred onto the XPS measurement stage. The binding energy was calibrated using the Si 2p (103.4eV).

# 2. 5 X-ray diffraction (XRD)

XRD measurement was recorded on a RIGAKU RU-3L equipped with a Co source (Co-K $\alpha$  radiation). Samples of catalyst powder were pressed into wafers and affixed to standard-sized microscope slides. Calculations of average crystallite size were made using the Pt(111) linewidth in Scherrer's equation with the Gaussian lineshape approximation.

# 2. 6 Chemisorption of CO

Chemisorption measurement of CO was carried

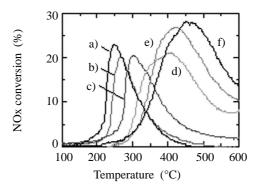
out by a pulse technique with chromatographic analysis. Catalyst samples placed in a flow reactor were pretreated at  $400^{\circ}$ C for 15 min in flowing  $H_2$  and cooled to  $25^{\circ}$ C. After that, several pulses of CO were introduced to the reactor until equilibrium was reached. The surface dispersion of Pt was calculated assuming that one molecule of CO adsorbs on an atom of Pt.

### 3. Results and discussion

# 3. 1 Catalytic activity under excess oxygen conditions

Fig. 1 shows the conversions of  $NO_x$  on PS, PNS, PMS, PMNS1, PMNS2, and PMNS3 catalysts in a simulated oxidizing feedstream as a function of temperature. The PS and PNS catalysts showed maximum conversions of NO<sub>x</sub> at temperatures from 250 to 260°C. The conversions of NO<sub>x</sub> by these catalysts rapidly decreased with increasing temperature above 260°C. The temperature of the maximum NO<sub>x</sub> conversion (300°C) on the PMS catalyst was about 50°C higher than that on the PS catalyst. The conversion of NO<sub>x</sub> gradually decreased with increasing temperature above 300°C. On the other hand, the maximum NO<sub>x</sub> conversion temperatures (400~450°C) on the PMNS1, PMNS2 and PMNS3 catalysts were about 150 to 250°C higher than that on the PS catalyst.

**Fig. 2** shows the conversions of  $NO_x$  on the PMLS, PMKS, PMMS and PMCS catalysts as a function of temperature. The PMLS and PMKS



**Fig. 1** NO<sub>x</sub> conversion efficiency as a function of temperature in simulated oxidizing feedstream. The following catalysts are indicated: a) PS, b) PNS, c) PMS, d) PMNS1, e) PMNS2 and f) PMNS3.

catalysts showed maximum conversion of  $NO_x$  at temperatures from 400 to  $500^{\circ}$ C. The temperature dependence of  $NO_x$  conversion on these catalysts had features similar to those of the PMNS2 catalyst in Fig. 1. On the other hand, the PMMS and PMCS catalysts showed maximum conversion of  $NO_x$  below 350°C, and the features were similar to those the PMS catalyst in Fig. 1.

**Fig. 3** shows the conversions of NO<sub>x</sub> on PMNA, PMNT, PMNZ and PMNs catalysts as a function of temperature. The PMNA and PMNT catalysts showed maximum conversions of NO<sub>x</sub> below 300°C and had features similar to those of the PMS catalyst. The conversions of NOx on PMNZ and PMNs catalysts were higher than those of the PMNA and PMNT catalysts at temperatures from 400 to 500°C. However, the NO<sub>x</sub> conversion curves of these catalysts were not similar to that of the PMNS2 catalyst.

MS and NS catalysts do not have activity for  $NO_x$  reduction in a simulated oxidizing feedstream in a temperature range under  $600^{\circ}$ C.

As shown in Figs. 1-3, the NO<sub>x</sub> conversion curves are classified into three groups: The first group is composed of the NO<sub>x</sub> conversion curves on the catalysts without Mo such as the PS and PNS catalysts, the second group is of that on the catalyst with Mo and without alkaline metal or an SiO<sub>2</sub> support such as the PMS, PMMS, PMCS, PMNA, PMNT, PMNZ and PMNs catalysts, and the third group is of those on the catalysts with Mo, alkaline metals and an SiO<sub>2</sub> support such as the PMNS1,

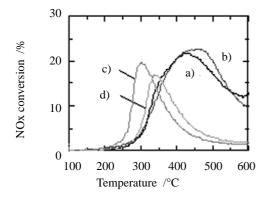


Fig. 2 NO<sub>x</sub> conversion efficiency as a function of temperature in simulated oxidizing feedstream.
a) PMLS, b) PMKS, c) PMMS and d) PMCS.

PMNS2, PMNS3, PMLS and PMKS catalysts.

In the first group, the PS and PNS catalysts show maximum conversion of  $NO_x$  at temperatures from 250 to 260°C. This temperature dependence of  $NO_x$  selective reduction had already been described<sup>5-7)</sup>. This result indicates that the addition of Na to the PS catalyst does not play a significant role in the reactivity of Pt on the PNS catalyst.

In the second group, the maximum  $NO_x$  conversion temperature (300°C) is about 50°C higher than those on PS catalyst. The conversion of  $NO_x$  gradually decreases with increasing temperature above 300°C. These results indicate that the addition of Mo plays a significant role in the reactivity of Pt catalysts.

In the third group, the maximum  $NO_x$  conversion temperatures (400~450°C) are about 150 to 250°C higher than those on PS catalyst as shown in Figs. 1 and 2. The maximum  $NO_x$  conversion and its temperature on PMNS1, PMNS2 and PMNS3 catalysts increase with increasing amount of Na added to these catalysts as shown in Fig. 1. These results indicate that the addition of Mo and alkaline metals plays a significant role in the reactivity of Pt on an  $SiO_2$  support.

A number of papers had already described that the temperature of the maximum NO<sub>x</sub> conversion for selective reduction of NO<sub>x</sub> on Pt catalysts changed with the Pt loading<sup>7)</sup>, the Pt precursor<sup>8)</sup>, and the aging conditions. In these cases, the maximum NO<sub>x</sub> conversion decreased with increasing temperature, which has been explained by the changing of the

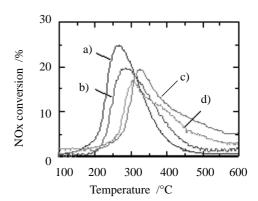


Fig. 3 NO<sub>x</sub> conversion efficiency as a function of temperature in simulated oxidizing feedstream.
a) PMNA, b) PMNT, c) PMNZ and d) PMNs.

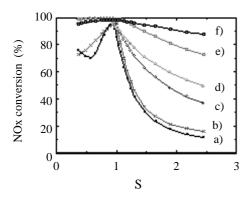
number of active sites on Pt. On the other hand, for selective reduction of  $NO_x$  on the catalysts in the third group, the maximum  $NO_x$  conversion increases as the temperature increases. This result can be explained by the improvement in the reaction characteristics of Pt inherent in the addition of Mo and alkaline metals, as mentioned below.

# 3. 2 Catalytic activity near the stoichiometric point

**Fig. 4** shows the conversions of NO<sub>x</sub> at 450°C on the PS, PNS, PMS, PMNS1, PMNS2 and PMNS3 catalysts, respectively, when *S* changes from reducing to oxidizing conditions around the stoichiometric point. The reaction temperature was chosen as 450°C at which the effect of the addition of Mo and Na appeared. All the catalysts have high conversion activity of NO<sub>x</sub> when *S* is nearly equal to 1. The NO<sub>x</sub> conversion curves are also classified into the three groups described above.

In the first group, the PS and PNS catalysts show poor  $NO_x$  conversion activity except for around the stoichiometric point (S=1). This characteristic feature is the same as that of the supported Pt catalysts reported previously<sup>23</sup>. It is assumed that NO reductions inhibited by  $O_2$  and  $CO^{31}$  adsorbed on Pt under lean and rich conditions, respectively.

In the second group, the PMS catalyst has higher  $NO_x$  conversion activity than the catalysts of the first group. As shown in Fig. 4, the addition of Mo has the effect of enhancing the  $NO_x$  reduction activity under lean and rich conditions compared with the PS and PNS catalysts. Gandhi and Shelef et al.<sup>23-25)</sup> had



**Fig. 4** NO<sub>x</sub> conversion efficiency as a function of redox ratio in simulated exhaust for *S*-scan at 450 °C. The following catalysts are indicated: a) PS, b) PNS, c) PMS, d) PMNS1, e) PMNS2 and f) PMNS3.

already described similar results in which Mo in  $PtMo/Al_2O_3$  and  $PdMo/Al_2O_3$  catalysts improved  $NO_x$  reduction under slight lean conditions compared with  $Pt/Al_2O_3$  and  $Pd/Al_2O_3$  catalysts.

In the third group, the PMNS1, PMNS2 and PMNS3 catalysts show much higher conversion in S > 1, compared with the catalysts without Mo or Na in the first and second groups. As shown in Fig. 4, the conversion of NO<sub>x</sub> on the PMNS1, PMNS2 and PMNS3 catalysts under rich, lean and stoichiometric conditions increase with the increasing addition of Na. When 1 wt% Na<sub>2</sub>O (PMNS3 catalyst) is added, the conversion of  $NO_x$  was over 90 % at 0.36 < S <2.45. This result indicates that Na and Mo on a Pt catalyst improves the conversion of NO<sub>x</sub> more significantly than Mo on a Pt catalyst. It is suggested that the addition of Mo and Na to a Pt catalysts has the effect of expanding the active S window in which three-way activity occurs, in particular, the window of the conversion of NO<sub>x</sub>.

The MS and NS catalysts do not have activity for  $NO_x$  reduction when S changes gradually from reducing to oxidizing conditions around the stoichiometric point at 450 °C.

### 3. 3 Selectivity of NO

NO selectivity, for the selective reduction of  $NO_x$  in the presence of excess oxygen, is given by the following expression.

NO selectivity =  $\frac{NO\_\ consumption}{NO\_\ consumption + O_2\_\ consumption} \times 100(\%)$ 

\_ consumption (2)

Fig. 5 shows the NO selectivity in the model gas

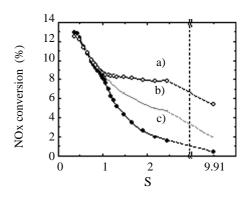


Fig. 5 NO selectivity for NO reduction as a function of redox ratio in simulated exhaust for *S*-scan at 600 °C. The following catalysts are indicated: a) PMN3 and b) PS. C) indicates partial pressure ratio of NO in inlet NO and O<sub>2</sub> gases.

reaction at 450°C when S changes from 0.36 to 9.91. In Fig. 5, no symboled line indicates the partial pressure ratio of NO in the inlet NO and O2 gases. At S < 1, the NO selectivity of both PS and PMNS3 is nearly the same as the partial pressure ratio of NO in the inlet NO and O2 gases. This result indicates that NO functions as an oxidant as dose oxygen at S<1. At S>1, the NO selectivity of PS is less than the partial pressure ratio of NO, while, the NO selectivity of the PMNS3 catalyst is higher than the partial pressure ratio of NO at S>1. Thus, the PtMoNa/SiO<sub>2</sub> catalyst has the feature that the reaction in which oxygen participates is inhibited by excess oxygen, so that the reaction in which NO participates as an oxidant proceeds preferentially. The effect of the inhibition of the reaction induced by  $O_2$  is assumed to lead to widening of the S window of NO<sub>x</sub> reduction activity around the stoichiometric point and the enhancement of NO<sub>x</sub> reduction activity under lean conditions.

## 3. 4 Characterization of catalysts

We examined the oxidation state of Pt on PS, PMS, PMNS2 and PMNS3 catalysts by an IR study using CO as a probe molecule. Table 2 shows the wavenumbers of the stretching vibration of CO adsorbed on Pt,  $\nu$  (CO<sub>ads</sub>), when the catalysts were pretreated in flowing 7 % O<sub>2</sub>/N<sub>2</sub>, 100 % N<sub>2</sub> and 7 % H<sub>2</sub>/N<sub>2</sub>, respectively, before IR measurement. In the measurement of Mo-containing catalysts, the intensity of diffuse reflectance IR was too weak to determine the position of wavenumbers of  $\nu$  (CO<sub>ads</sub>). As for the PS catalyst, the positive shift of wavenumbers of  $\nu$  (CO<sub>ads</sub>) is large in the order of flow of 7 %  $O_2/N_2$ , 100 %  $N_2$  and 7 %  $H_2/N_2$ . These results indicate that Pt exists in a high oxidation state under oxidizing conditions and exists in a low oxidation state under reducing conditions. On the other hand, the PMS, PMNS2 and PMNS3 catalysts

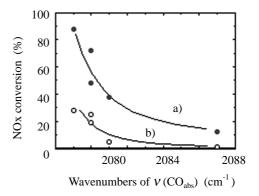
**Table 2** The wavenumbers of  $\nu$  (CO<sub>ads</sub>).

Catalyst		wavenumbers (cm <sup>-1</sup> ) pretreatment ( balance, N <sub>2</sub> )			
	$O_2$	$N_2$	$H_2$		
PS	2087	2079	2074		
PMS	2081	2078	-		
PMNS2	2080	2075	-		
PMNS3	2079	2075	-		

have a negative shift compared with the PS catalyst. The difference in wavenumbers in  $\nu$  (CO<sub>ads</sub>) on PtMoNa/SiO<sub>2</sub> after N<sub>2</sub> pretreatment and after O<sub>2</sub> pretreatment was less than that on the PS catalyst, and the wavenumbers of  $\nu$  (CO<sub>ads</sub>) obtained on the PMS, PMNS2 and PMNS3 catalysts after O<sub>2</sub> pretreatment are similar to that on the PS catalyst after N<sub>2</sub> pretreatment. These results suggest that the electron density of the Pt atoms of PtMoNa/SiO<sub>2</sub> are maintained at a high level even under oxidizing conditions and that oxidation of Pt is inhibited.

**Fig. 6** shows the relation between the wavenumbers of  $\nu$  (CO<sub>ads</sub>) after O<sub>2</sub> pretreatment and the conversion of NO<sub>x</sub> on the PtMoNa/SiO<sub>2</sub> catalyst at 450°C. When S is 2.45 and 9.91, the conversion of NO<sub>x</sub> at 450°C becomes higher as the wavenumbers of  $\nu$  (CO<sub>ads</sub>) become lower. It is derived from this result that inhibition of the oxidation of Pt on the PtMoNa/SiO<sub>2</sub> catalysts caused increasing NO<sub>x</sub> reduction activity.

The study of the oxidation state of Pt by XPS leads to the same conclusion mentioned above. **Fig. 7** shows the XPS spectra in the region of the Pt  $4f_{7/2}$  emission band of the Mo-containing catalyst, such as PMS, PMNS2 and PMNS3 catalysts after  $O_2$  pretreatment. The addition of Na causes a negative shift in the Pt  $4f_{7/2}$  binding energy of the PtMoNa/Si $O_2$  catalysts. XPS spectra measured under oxidizing conditions also clarify that Pt on



**Fig. 6** The relation between the wavenumbers of v (  $CO_{ads}$  ) after  $O_2$  pretreatment and  $NO_x$  conversion on the PtMoNa/Si $O_2$  catalyst at 450°C. The following redox ratio, S, are indicated: a) 2.45 ( simulated A/F = 15.2 ) and b) 9.91 ( simulated A/F = 18 ).

PMNS2 and PMNS3 catalysts is difficult to oxidize even under substantially O<sub>2</sub>-rich conditions and the oxidation state of Pt becomes lower with increasing Na content.

Table 3 shows the amount of CO adsorbed on the catalysts under reducing conditions. As for the PS and PNS catalysts, the amount of CO adsorbed on the catalyst is relatively large. This result indicates that a large amount of Pt exists on the surface of the catalyst. On the other hand, the catalysts including only Mo lose their ability to chemisorb CO, and the CO-to-Pt ratio (CO/Pt) becomes lower with increasing Na content, while XRD patterns show no crystalline Pt on the PtMoNa/SiO<sub>2</sub> catalysts in the third group. These results are in agreement with the model that Tri et al. <sup>26)</sup> have already reported. As they have pointed out, it seems reasonable to suppose that physical masking around Pt atoms is

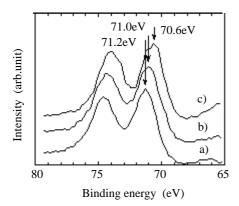


Fig. 7 XPS spectra of Pt 4f after  $O_2$  pretreatment  $(1 \times 10^{-7} \text{ torr } O_2, 1\text{h})$ . The following catalysts are indicated: a) PMS, b) PMNS2 and c) PMNS3.

**Table 3** Amounts of CO adsorbed on catalysts.

Catalyst	adsorbed CO μmol/g-cat	CO/Pt ratio mol/mol
PS	32.8	38.4
PNS	29.0	33.9
PMS	1.9	2.2
PMNS1	1.5	1.7
PMNS2	0.6	0.7
PMNS3	0.3	0.4

caused by the Mo atoms deposited on the surface of the Pt atoms under reducing conditions. In addition, EXAFS and XPS analyses of PtMo/SiO<sub>2</sub> catalysts reported by Liu et al. <sup>28)</sup> also support this model. In our case, as Na is added to PtMo/SiO<sub>2</sub> catalyst, Na probably assists Mo in masking more widely around the Pt atoms. Such an assumption is supported by the decrease in the amount of adsorbed CO.

# 3. 5 The possible reason for the change in catalytic performance in PtMoNa/SiO<sub>2</sub>

Only the Mo-supported catalyst and only the Nasupported catalyst showed no activity for  $NO_x$  reduction. Therefore, the active center of PtMoNa/SiO<sub>2</sub> is Pt, which determines the catalytic performance of  $NO_x$  reduction. The effect of the addition of Mo and Na is estimated to change the reaction characteristics of the Pt.

From the IR spectra of adsorbed CO and XPS spectra, it is demonstrated that the oxidation state of Pt on PtMoNa/SiO<sub>2</sub> catalysts is lower than that on the PS catalyst, that Na content strongly affects the oxidation state of Pt on PtMoNa/SiO<sub>2</sub> catalysts and that the oxidation state of Pt has a correlation with NO<sub>x</sub> reduction activity. Further, the estimation of NO selectivity reveals that the PtMoNa/SiO<sub>2</sub> catalyst has the feature that the reaction in which oxygen participates was inhibited in the presence of excess oxygen.

These results described above can possibly be explained by the assumption that the oxidation of Pt corresponds to the activation of O2 which leads to the oxidation of NO and reductants such as C<sub>3</sub>H<sub>6</sub>, CO and H<sub>2</sub>. It is assumed that the adsorption or dissociation of  $O_2$  causes oxidation of Pt and that  $O_2$ becomes activated for the oxidation reaction through the adsorption and dissociation. In general, the dissociation rate of adsorbed O2 is faster than that of adsorbed NO on a Pt surface 32), so that NO is a weaker oxidant than O2 on the Pt surface and NO functions rather as a reductant and reacts with O2 to produce NO<sub>2</sub> in the presence of excess oxygen. However, the addition of Mo and Na changes the characteristics of Pt under the conditions where oxygen sufficiently functions as an oxidant, so that the activation of O<sub>2</sub> is inhibited and NO is easily reduced. The reason for this is assumed to be the lower affinity between Pt and oxygen caused by the addition of Mo and Na.

From such structural information on PtMoNa/SiO<sub>2</sub>

catalysts, it is concluded that a physical masking by Mo and Na exists around Pt, as mentioned before. Cáseres et al. have reported that MoO<sub>3</sub> exists in a poorly dispersed form and has a high reducibility on an SiO<sub>2</sub> support compared with other supports<sup>33)</sup>.

Perhaps, on the SiO<sub>2</sub> support, MoO<sub>3</sub>, which has high reducibility, interacts physically or chemically with Pt and the interaction assisted by the addition of Na affects the electron density of the Pt atoms. As described above, Pt atoms on the PtMoNa/SiO<sub>2</sub> catalysts retains a high electron density even under excess oxygen conditions and accordingly resists oxidation. Under such environmental conditions, Pt atoms are assumed to be the active component of the characteristic NO<sub>x</sub> selective reduction as described above and previously<sup>35</sup>. It is assumed that the reason mentioned above explains not only the reactivity of the PtMoNa/SiO<sub>2</sub> but also that of PtMo/SiO<sub>2</sub> with alkaline metal additives such as Li and K instead of Na.

#### 4. Conclusions

This paper has described the effects of the addition of Mo, alkaline metals and alkaline earth metals to Pt catalysts on various supports, compared with PtMo/SiO<sub>2</sub>, PtNa/SiO<sub>2</sub> and Pt/SiO<sub>2</sub> catalysts. From the above results, we found that the PtMo/SiO<sub>2</sub> catalysts with alkaline metal additives have different characteristics from those of conventional Pt catalyst such as a Pt/SiO<sub>2</sub> catalyst. Some characteristics of PtMoNa/SiO<sub>2</sub> are described below.

- 1) Under lean static conditions, the temperature window of  $NO_x$  reduction of the PtMoNa/SiO<sub>2</sub> is wider than that of the Pt/SiO<sub>2</sub> catalyst.
- 2) Under nearly stoichiometric condition, the  $PtMoNa/SiO_2$  catalysts had wide redox ratio windows of  $NO_x$  reduction compared with the  $Pt/SiO_2$  catalyst.
- 3) The PtMoNa/SiO<sub>2</sub> catalysts have the reaction feature that NO is used selectively as an oxidant under oxidizing conditions.
- 4) The interaction of Mo and Na with Pt is assumed to lower the affinity between Pt and oxygen and results in the reaction characteristics of the PtMoNa/SiO<sub>2</sub> catalysts.

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